Design Procedures for Soil Modification or Stabilization

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January 5, 2020
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DESIGN PROCEDURES FOR SOIL MODIFICATION OR STABILIZATION

1.0 General

Indiana Department of Transportation’s policy is to minimize the disruption to motorists due to change in traffic patterns and traffic delays caused during the construction or reconstruction of the State’s roads and bridges. Indiana Department of Transportation (INDOT) is often faced with the difficulty of constructing roadbeds on or with soils, which do not possess the sufficient strength to support wheel loads imposed upon them during the construction or the service life of the pavement. At times it is necessary to treat these soils to provide a stable subgrade or a working platform for the construction of the pavement. These treatments require less time and energy in the production, handling, and placement of road and bridge fills and subgrades, therefore, reducing the disruption and delays to traffic.

These treatments are generally classified into two processes, soil modification or soil stabilization. The purpose of subgrade modification is to create a working platform for construction equipment. A small credit is accounted for this modification in the pavement. The purpose of subgrade stabilization is to enhance the strength of the subgrade and this increased strength is taken into account in the pavement design. Subgrade stabilization requires a more thorough design methodology during construction compared to subgrade modification. The methods of subgrade modification or stabilization include physical processes such as soil densification, blending with granular material, the use of reinforcement such as geosynthetics or undercutting and replacement. The treatment also includes chemical processes such as mixing with cement and lime. Soil properties such as strength, compressibility, hydraulic conductivity, workability, swelling potential, and volume change tendencies may be altered by various soil modification or stabilization methods. When designers require fast construction, soils with higher moisture contents can be dried with the use of chemical modifiers. When soil properties require alteration, these soils can be altered by performing chemical soil stabilization.

Subgrade modification shall be considered for all the reconstruction and new alignment projects. When used, modification or stabilization shall be required for the full roadbed width including shoulders and curbs. Subgrade stabilization shall be considered for all subgrade soils with a resilient modulus less than 5,000 psi based on laboratory testing.

INDOT Standard Specifications provide several options for subgrade treatment types which include chemical modification, replacement with aggregates, geosynthetic reinforcement in conjunction with the aggregates, density, and moisture control. The geotechnical engineer shall evaluate the needs of the subgrade and include where necessary, specific types of treatment beyond the requirements of Sec. 207 specification.

Various soil modification or stabilization guidelines are discussed below. Project location, local economic factors, as well as environmental conditions shall be considered in order to make prudent decisions for design. It is important to note that modification and stabilization terms are not interchangeable.
2.0 Modification or Stabilization of Soils

2.1 Mechanical Modification or Stabilization

Mechanical modification or stabilization is the process of altering soil properties by changing the gradation through mixing with other soils, densifying the soils using compaction efforts, or undercutting the existing soils and replacing them with granular material.

A common remedial procedure for wet and soft subgrade is to cover it with granular material or to partially remove and replace the wet subgrade with a granular material to a pre-determined depth below the grade lines. The compacted granular layer distributes the wheel loads over a wider area and more evenly distributes wheel loads serves as a working platform.

To provide a stable working platform using granular material, the following conditions shall be met.

1. The thickness of the granular material must be sufficient to develop acceptable pressure distribution over the wet/soft soils.
2. The backfill material must be able to withstand the wheel load without rutting.
3. The compaction of the backfill material shall be in accordance with the Standard Specifications.

Based on the results from research, usually 12 in. to 24 in. of granular material shall be adequate for subgrade stabilization. However, deeper undercut and replacement may be required in certain areas. Drainage improvement shall also be considered such as ditches or French drains.

The undercut and backfill option is widely used for construction traffic mobility and work platform. This option could be used either on the entire project or as a spot treatment. The equipment needed for construction is normally available on highway construction projects.

2.2 Geosynthetic Reinforcement

Geosynthetics have been used to reinforce road sections on INDOT projects. The inclusion of geosynthetics in subgrade has changed the performance of the roadway in many ways. Tensile reinforcement, confinement, lateral spreading reduction, separation, construction uniformity, and reduction in strain have been identified as primary reinforcement mechanisms. INDOT Standard Specification Section 207 and Section 214 specify the use of geotextile and geocell. Empirical design and post-construction evaluation have lumped the benefits into better pavement performance during the design life. The use of geotextile, geogrid, and geocell with a reduced aggregate thickness option has been successfully designed in urban areas with high water conditions.
Construct 12 in. of coarse aggregate subgrade with geogrid, geotextile, or geocell. This reinforced coarse aggregate shall provide a stable working platform.

Geotextiles, geogrids, and geocells shall be in accordance with 918 and be placed directly over exposed soils to be modified or stabilized and then overlapped in accordance with the following table.

<table>
<thead>
<tr>
<th>Dynamic Cone Penetration Blow Counts per 6 inches</th>
<th>Overlap</th>
</tr>
</thead>
<tbody>
<tr>
<td>&gt; 5</td>
<td>12 in.</td>
</tr>
<tr>
<td>3 to 5</td>
<td>18 in.</td>
</tr>
<tr>
<td>less than 3</td>
<td>24 in.</td>
</tr>
</tbody>
</table>

Table 1: DCP Blow Counts per 6 Inches and Geogrid Overlap

2.3 Chemical Modification or Stabilization

The addition of chemicals such as cement, fly ash, or lime alter the physical and chemical properties of the soil. There are the two primary mechanisms by which chemicals alter the soil into a stable subgrade:

1. Increase in particle size by cementation, reduction in plasticity index, increased internal friction among the agglomerates, greater shear strength, and lower shrink/swell potential.

2. Absorption and chemical binding of moisture that will facilitate compaction.

3.0 Design Procedures

3.1 Suggested Criteria for Chemical Selection

When the chemical stabilization or modification of subgrade soil is considered the most feasible alternative, the following criteria shall be considered for chemical selection based on the index properties of the soils.

   
   a. Lime\(^1\): Clay content > 30 % and PI > 20.
   
   b. Cement: Clay content ≤ 30% and PI ≤ 20.

2. Chemical Selection for Modification
   
   a. Lime: Clay content > 30% and PI >20.
b. Cement: Clay content ≤ 30% and PI ≤ 20.

Note 1. Lime shall be quick, hydrated lime, or by-product and shall have a soluble sulfate content < 5%.
Note 2. In lieu of lime class C fly ash with a soluble sulfate content < 5% may be used.
Note 3. When fly ash class C is substituted in lieu of lime, a minimum corresponding strength of 50 psi gain should be obtained.

Note 4. Use of fly ash is not permitted between October 15 and April 15. Appropriate tests showing the improvements in the strength gain and the swell reduction are essential for the exceptions listed above.

Note 5 Lime treated soils may not provide immediate stability due to presence of high-moisture. Geotechnical consultants may recommend cement as modifier for faster strength gain in these conditions.

3.2 Suggested Chemical Quantities for Modification or Stabilization

1. Lime or Lime By-Products: 5% to 7%
2. Cement: 5% to 8%
3. Fly ash: 10% to 15%

3.3 Suitable Soils for Modification or Stabilization

The reaction of a soil with lime, cement, or fly ash is important for stabilization and modification. Design methodology shall be based on an increase in the unconfined compressive strength of the mixture. A pair of specimens of 3in. diameter by 6 in. height with a ratio of 2:1, height/diameter, is prepared at 95% of the standard Proctor and the optimum moisture content. A 5% cement, 6% lime or 10% fly ash can be used in soils mixture. These specimens are cured for 48 hours at 70°F in the laboratory and tested in accordance with AASHTO T-208. A complimentary set of two specimens are also prepared of the soil at 95% of standard Proctor and optimum moisture content. All specimens are then subjected to unconfined compressive testing. The minimum strength gain of both samples of the lime-soil mixture shall be 50 psi over that of the natural soil. When the contractor chooses to use slurry. The soils chemical modifier the specimen should be molded at the natural moisture content of the subgrade soils.

The minimum strength gain of the cement-soil mixture shall be 100 psi over that of the natural soil mixture and minimum strength gain for the fly ash-soil mixture shall be 50 psi over that of the natural soils.
4.0 **Laboratory Test Requirements**

Soil modification or stabilization mix design shall be performed in accordance with the following: AASHTO T 88, T 89, T 90 T 89, T 90, T 99, T 208, T 265, T 289, T 307, and ITM 510. All the tests shall be performed in AMRL inspected laboratory.

4.1 **Soil Sampling.**

An approved Geotechnical Engineer shall visit the project during the construction and collect a bag sample of each type of soil in sufficient quantity for performing the specified tests. The Geotechnical Engineer shall review the project geotechnical report and other pertinent documents, including soil maps, etc. prior to the field visit. The Geotechnical Consultant shall submit the test results and recommendations, along with the current material safety data sheet and evidence that modifier is from INDOT approved list to the Engineer for approval. If the Geotechnical Engineer determines the necessity of chemical-soil stabilization during the design phase, they shall design a subgrade treatment utilizing the chemical in the geotechnical report in accordance with INDOT guidelines. Following properties shall be checked prior to any modification or stabilization.

2. pH test for optimum lime content determination with the exceptions listed below
3. Perform the suitability test as required in Sec 3.3
4. Max. Dry unit weight of 90pcf (min.) or greater,
5. Loss on Ignition*1 (LOI) not more than 6 % dry weight of soil
6. Sulfate content shall not be more than 1,000 ppm
7. Two unconfined strength on 95% compacted soils
8. Two unconfined test on 95% chemically modified specimen
9. Two resilient modulus*2 on chemically modified (for stabilization) soils

Note 1: Loss on Ignition tests shall be performed when required.

Note 2: Mr Test would be performed during design phase and two specimens shall be sent to the Office of Geotechnical Services for testing. The Geotechnical Consultants shall coordinate with the INDOT Geotechnical Lab Supervisor for the sample size and dimensions needed to perform Mr Test.

4.2 **Lime or Lime By-Products Required for Modification or Stabilization**
Lime reacts with fine grained soils, clay, to produce decreased plasticity, increased workability, reduced swell and increased strength. As a general guide, treated soils shall increase in particle size by cementation, reduction in plasticity, increased in internal friction among the agglomerates, greater shear strength, and increased workability due to the textural change from plastic clay to a friable, sand like material.

The following procedures shall be utilized to determine the amount of lime required to chemically treat the subgrade. Hydrated quick lime or lime by-products 5 to 7% by weight, shall be used for soil modification or stabilization. The following procedures shall be used to determine the optimum lime content.

1. The sieve analyses on the soils shall be performed.
2. The separate pH of soil and lime samples shall be determined.
3. The optimum lime content using Eades and Grim pH test shall be determined as follows:
   a. 20 g of oven-dried minus No. 40 soil shall be weighed to the nearest 0.1 g and poured into 150-ml, or larger, plastic bottles with screw tops.
   b. A sufficient amount of lime shall be added to soils to produce a pH of 12.4 or equal to the pH of the lime before mixing. A graph shall be plotted between the pH value and the lime percentage. The optimum lime content shall be determined corresponding to the maximum pH of lime-soil mixture. See Figure 1. It is advisable to set up five bottles with lime percentages of 3, 4, 5, 6, and 7. This shall ensure, in most cases, that the percentage of lime required can be determined in one hour. Weigh the lime to the nearest 0.01 g and add it to the soil. Shake to mix soil and dry lime.
   c. 100 ml of CO₂-free distilled water shall be added to the bottles to the bottles.
   d. The soil, lime, and water mixture shall be shaken until there is no evidence of dry material on the bottom. Shake for a minimum of 30 seconds.
   e. The bottles shall be shaken for 30 seconds every 10 minutes for one hour.
   f. After one hour, part of the slurry shall be transferred to a plastic beaker and the pH shall be measured. The pH meter shall be equipped with a Hyalk electrode and standardized with a buffer solution having a pH of 12.00.
   g. The pH for each of the lime-soil mixtures shall be recorded. If the pH readings reach 12.40, the lowest percentage of lime that yields a pH of 12.40 is the percent required to stabilize the soil. If the pH does not go beyond 12.30 whereas 2 percent lime produces the same reading, the lowest percent which gives a pH of 12.30 is that required to stabilize the soil. If the highest pH is 12.30 and only 1 percent lime
gives a pH of 12.30, additional test bottles shall be started with larger percentages of lime.

h. An Atterberg limit test shall be performed on soil and lime mixture corresponding to optimum lime content.

i. Compaction testing shall be performed on the optimum lime and soil mixture to evaluate the drop in maximum dry density in relation to lime.

j. A pair of lime treated specimens compacted at 95% of Proctor, shall be tested for strength at 70º F after curing for 48 hours. The strength gain shall be at least 50 psi over the natural soils.

**Figure 1: pH vs. Lime Content**

![pH vs Lime Content graph](image)

In the case of stabilization, two prepared specimens shall be delivered to the Division of Geotechnical Services for Resilient Modulus testing. Resilient Modulus \((M_R)\) at 95% compaction, shall be performed in addition to the above tests corresponding to optimum lime and soil mixture of predominant soils types.

### 4.3 Cement Required for Stabilization or Modification

The following methodology shall be used for quality control and soil cement stabilization. 5-8 % of cement can be utilized to modify the subgrade.

1. Perform the mechanical and physical properties of the soils.
### AASHTO Classification

<table>
<thead>
<tr>
<th>AASHTO Classification</th>
<th>Typical Range Of Cement Percentage by Dry Weight of Soil</th>
</tr>
</thead>
<tbody>
<tr>
<td>A-1, A-3</td>
<td>5 – 7</td>
</tr>
<tr>
<td>A-2, A-4</td>
<td>5 - 6</td>
</tr>
</tbody>
</table>

**Table 2: AASHTO Classifications for Cement Requirements**

2. Perform the standard Proctor on soil-cement mixture. Prepare 2 specimens, as per 3.3. The strength gain shall be at least 100 psi when compared to the natural pills.

3. The resilient modulus shall be determined on the two specimens molded at 95% of the Standard Proctor for soil treated with cement. A strength gain of 100 psi is adequate enough to allow for stabilization at 48 h at 70º F and % cement shall be adjusted.

### 4.4 Fly Ash Required for Modification

1. The in-situ soils shall meet the criteria of modifications.

2. Standard Proctor shall be performed to determine the maximum dry density and optimum moisture content of the soil.

3. Fly ash shall be mixed with the soils in increments of 10%, 15%, and 20% by dry weight. Each blend of the mixture shall be tested per standard Proctor to determine their respective maximum dry densities.

4. The compaction of mixes shall be completed within 2 hours of mixing.

5. A percentage of fly ash, which provides the highest maximum dry density, shall be considered as the optimum amount of fly ash for that soil.

6. Unconfined compressive strength of optimum fly ash mix sample shall be determined on a pair of specimens at 95% of the standard Proctor which have been cured at 70º F for 48 hours. The strength gain shall be a minimum of 50 psi.

7. Two specimens of optimum fly ash mix sample shall be molded for standard Proctor. The swell test shall be performed for extended period. The swelling shall be observed daily for 7 days. If the swell exceeds 3% then the chemical shall not be allowed to treat the soils tested.

### 4.5 Soils Drying

Lime is an effective chemical modifier in soil moisture reduction. The presence of free calcium in chemical modifier makes soils drier, increases optimum moisture content of the soils in addition to changes in other soils properties. The moisture reduction by hydration and increase in optimum moisture content make this application very attractive for designers to plan ahead an expedited construction schedule. Lime application affects soils in the following manner:
• Dilution: adding dry chemical to wet soils

• Calcium Oxide Hydration: Rapid hydration of calcium oxide to calcium hydroxide,

• Evaporation: The exothermic reaction of lime hydration increases moisture reduction.

• Pozolonic Reaction: Moisture combine into alumina silica compounds as pozolonic reaction begins, therefore there moisture reduction due to pozolonic reaction.

• Optimum Moisture Content (OMC) Change: An increase of OMC due to flocculation/ agglomeration based on a change in texture from parallel alignment to edge to face attraction. The new texture will have more voids and additional room for any increase in moisture.

The following procedure shall be used to determine the appropriate modifier as well as develop a relationship with moisture range and time delays so the modifier adjustment can be made during construction if needed.

1. All of the tests shall be performed at room temperature or at temperature desired by the Geotechnical Engineer.

2. Collect a jar soil sample of the in-situ soil and determine the in-place moisture content of the soil.

3. Perform mechanical and physical tests on each soil sample along with Loss on Ignition, if required.

4. Perform the sulfate test on each soil sample.

5. Determine the pH of soil and lime samples separately.

6. Perform a typical moisture-density test on each soil type.

7. Perform a typical moisture-density test on each soil and lime mixture, such as soils with 3% lime, soils with 4% lime etc. For example: soils that are 8% over OMC. After soils are mixed with 3%, 4% and 5% lime moisture content tests shall be performed each hour. Geotechnical consultant should not recommend over 5% lime kiln dust for drying application.

8. When wet soils encountered it should be spread and mixed with rotary speed mixers for moisture reduction.

9. Chemical modifier % vs. moisture content relationship shall be developed and presented in a tabular or graphical form so that the chemical modifier may be adjusted in the field, if needed, based on the in-situ soil moisture content. The table may be expanded to include additional time.

10. Compaction shall be performed on each lime-soil mixture to evaluate the drop in maximum dry density and the rise in optimum moisture content with respect to time (depending on the delay between the lime-soil mixing and compaction.)
<table>
<thead>
<tr>
<th>Soil ID</th>
<th>% Above OMC (Untreated)</th>
<th>Untreated MC</th>
<th>Treated MC (By Dry Weight) After one Hour</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>3%</td>
</tr>
<tr>
<td>Sta. 16+00</td>
<td>2</td>
<td>17.3</td>
<td>15.8</td>
</tr>
<tr>
<td>Sta. 16+00</td>
<td>4</td>
<td>19.5</td>
<td>18.0</td>
</tr>
<tr>
<td>Sta. 16+00</td>
<td>6</td>
<td>21.2</td>
<td>20</td>
</tr>
<tr>
<td>Sta. 16+00</td>
<td>8</td>
<td>23.8</td>
<td>22</td>
</tr>
</tbody>
</table>

**Table 3: Moisture Reduction vs. Lime**

### 4.6 Requirements for Geotechnical Submittals to INDOT

The mix design report shall be prepared by the INDOT Approved Geotechnical Consultant laboratory and duly signed by an Indiana Licensed Professional Engineer. The laboratory shall be inspected by AMRL. The summarized results of the mix design along with details shall include the following information:

1. Subgrade and its foundation (project Geotechnical report) review by Geotechnical Engineer
2. Textural and AASHTO Classifications of soils
3. Natural moisture content of soils
4. Soluble sulfate content
5. pH of soils
6. Atterberg limit of soils
7. Type and source of the chemical modifier or stabilizer
8. Mix design proportions
10. Unconfined compressive strength at 95% compaction of soil
11. Standard Proctor of chemically treated soils
12. Unconfined compressive strength of chemically treated soil specimens prepared at 95% compaction
13. Recommendations for mixing, pulverization, compaction and curing
14. Recommendations for guidance to maintain adequate moisture during mixing and curing
15. Confirmation that sulfate or other chemical constituents which may cause soil heaving are not present in the ground water. Water shall meet the requirement of Section 913.
16. Identify the specific limits of unstable foundation soils by reviewing the project geotechnical recommendations.
5.0 Construction Considerations

Modification of soils such as drying out of wet subgrade with lime, cement, and fly ash to speed construction is not as critical as completely stabilizing the soil to be used as a part of the pavement structure. With the growth of chemical modification throughout the state, a variety of applications are being suggested due to such factors as type of soil, percentage of modification/stabilization required, environmental constraints, and availability of chemicals. Furthermore, when chemically stabilized subgrade is used to reduce the overall thickness, the stabilized layer must be built under tight construction specifications, whereas requirements for the construction of working platforms are more lenient. Following are a few recommendations for modification or stabilization of subgrade soils.

1. Perform recommended tests on each soil to see if the soil will react with chemicals then determine the amount of the chemical necessary to produce the desired results.
2. Gradation and moisture test shall be performed in accordance with ITM 516 and ITM 506.
3. More chemicals may not give the best results.
4. Sulfate when mixed with calcium will expand. Soils having over 1,000 ppm sulfate content shall not be mixed with chemicals.
5. Soluble sulfate in lime and fly ash shall not be greater than 5%.
6. Chemical modifier shall be from INDOT approved list.
7. One increment of the chemical is recommended to produce a working platform.
8. Dynamic cone penetrometer (DCP) or Light Weight Deflectometer (LWD) shall be used in accordance with ITM 508 or ITM 509. Compaction acceptance shall be in accordance with 215.
9. Proof rolling shall be performed in accordance with 203.26 prior to placing a subsequent layer.
10. Set the grade low to account for the swell in the lime. A swell factor of 10% is an approximate estimate.

11. Uniform distribution of chemical, throughout the soil is very important.

12. Uniform spreading and mixing are very important for chemical modification or stabilization. Gradation shall be checked in accordance with Section 215.08.

13. Curing takes 7 days of 50°F + weather for stabilization. No heavy construction equipment shall be allowed on the stabilized grade during the curing period.

14. The maximum dry density of the soil-lime mixture is lower than in untreated soils. Maximum dry density reduction of 3~5 pcf is common for a given compactive effort. It is, therefore, important that the laboratory provide appropriate density. Generally lime or lime by products reduces the soils moisture by dilution, lime hydration, evaporation, and pozzolanic reactions. See Figure 3.

15. Cover the modified or stabilized roadbed with pavement before suspending work for the winter.

16. Cement treated soils exhibit shrinkage cracks due to soil type, curing, chemical contents, etc. Therefore, it is recommended to provide surface sealing on stabilized subgrade after the curing period.

17. Moisture content of modified or stabilized subgrade shall be maintained above the optimum moisture content of modified subgrade during the curing.
18. Lime raises the pH of the soil. Phenolphthalein, a color sensitive indicator solution can be sprayed on the soil to determine the presence of lime. If lime is present, a reddish-pink color develops. See Figure 4.

**Figure 4: Lime Modified Subgrade Uniformity Determination by Phenolphthalein**

19. Because lime can cause chemical burns, safety gear, such as gloves, etc. shall be used during construction and inspection as well.
References:


Chemical Modification Flow

Appendix 1

Soil Testing

- T 265 Moisture
- T89/90 Gradation/Atterburg
- T 289 PH
- T 267 LOI
- ITM 510 Sulfate
- T99 Std. Proctor
- T 208 Strength @ 95% Comp.

Max dry unit weight ≤ 90 pcf
LOI ≥ 6 sulfate ≤ 1000 ppl

Meets Specifications

Continue and follow chart below


Clay ≤ 30% PI ≤ 20
Cement

Clay>30% PI>20
Lime

Does Not Meet Specifications

STOP: Cannot perform Chemical Modification Contact Division of Geotechnical Services

Got to Chart 2
Chemical Modification Flow Chart

Appendix 2

Lime or Cement

Soil + Lime

Seive Analyses
Atterberg Limit

T 99

T 208 at 95%
Comp.

Strength gain for Lime mod. soil \( \geq 50 \) psi

Soil + Cement

Seive Analyses
Atterberg Limit

T 99

T 208 at 95%
Comp.

Strength gain for Cement mod. soil \( \geq 100 \) psi