

Traders Point Lake Dam

Investigation Report

State ID 49-5

January 31, 2008

Submitted by

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Executive Summary

An investigation was performed on the Traders Point Lake dam on January 23, 2008. The dam is owned by Lakeside Improvement Association. It is classified by the DNR as a low hazard dam, but has several serious deficiencies as defined by the DNR. The dam is 18 feet high and 300 feet long with a crest width of 5 feet and impounds a 10 acre lake at normal pool.

On the date of the investigation, the weather was cold and dry. There had been a recent light snowfall preceding the inspection. The level of the lake was right at the crest of the principal spillway.

The embankment is generally in good condition and the investigation centered on the structural condition of the concrete spillway, which has serious concrete failure problems.

It is recommended that the Owner give consideration to upgrading this structure to comply with current DNR standards of dams of this size and repair or replace the spillway as funding permits. Several options are presented in the report.

Dam Investigation

Data Reviewed

Prior to the field investigation on January 23, 2008, the immediate past DNR inspection report was reviewed.

Scope of Investigation

This investigation was to evaluate the structural condition of the principal spillway of the Traders Point Lake. It was limited to a visual observation of the field conditions, and an office review of those observations in order to provide a preliminary estimate for the cost of repairs. Extensive concrete and foundation sampling was not performed. This evaluation does not provide any guarantee of future safety or integrity of the dam beyond the investigation date.

Investigation Conditions

The spillway was field inspected on January 23, 2008 at approximately 1:30 pm. The conditions were cold and dry. The temperature was approximately 20degrees. There had been a recent snowfall, but it did not obstruct a clear view of the spillway. The water level was slightly above the crest of the principal spillway. Ice was observed at the left side of the spillway, both at the crest and on the wall.

Description of Dam and Spillway

This dam is located in Marion County, Indiana at the Traders Point Lake near 71st Street and Lafayette Road. It is a private dam and serves as an amenity for the development surrounding the lake. It appears in Section 27, T17N, R2E of the Zionsville USGS Quadrangle Map. Descriptive data for the dam and spillway is taken from the DNR Earth Dam Visual Inspection Report.

The dam is an earth filled structure, not approved by the DNR. The earthen embankment is approximately 18 feet high, 300 feet long and has slopes of approximately 1.5V:1H upstream and 3V:1H downstream. The principal spillway is a broad crested weir 2 feet thick, 30 feet wide, and 13.5 feet high. It has abutment walls on both sides and a wing wall on the left side. A wing wall probably existed on the right side but failed and no longer exists. The discharge is to a concrete impact slab and then a discharge channel.

The dam has an upstream drainage area of approximately 1.63 square miles and the permanent pool surface area is approximately 10 acres. The normal pool is 4.5 feet below the dam crest. There is approximately 4.5 feet of freeboard between the crest elevation and the spillway elevation.

Summary of Investigation

The spillway is spalled on the crest and downstream face. This spalling is repairable by chipping the remaining material down to sound concrete and rebuilding the crest and wall to the original dimensions. The right side abutment wall has spalled areas that are repairable by chipping the remaining material down to sound concrete and rebuilding the wall to the original dimensions. Please note that in some situations, sound concrete is never found during the chipping process and walls may need to be replaced. The center divider wall is also spalled and eroded and can be repaired by removing the deteriorated concrete and reconstructing the wall to the original dimensions. The left side abutment wall is in serious structural condition.

The left side abutment wall has an extensive crack that is not repairable. This wall also has several leaks. These leaks were defined by the evidence of water leaking through the wall and freezing, leaving significant ice formations. This wall also probably had a downstream wing wall that failed and is no longer present. There was some evidence that the wing wall remains are partially buried in the downstream stream bank. While efforts to repair this wall could be made, total replacement is the only repair that will likely be permanent.

The impact slab also has deteriorated concrete as a result of years of wear, but this damage can be repaired by removing the spalled and weak material and constructing an overlay.

Cost of Repairs

An estimate of the cost of repairs as identified was made. The cost is approximately \$150,000, if no hidden defects are discovered during the excavation, spalled concrete repair, and demolition. The repair will also require the draining of the lake during construction. The lake will be lost for approximately one year. If there are fish in the lake, it will take another three years after restocking for fingerlings to reach a size that would allow them to be caught.

As the current DNR inspection report also requested a hydraulic evaluation, a preliminary hydraulic model was constructed. The results of this study are reported below and have an impact on repair costs.

The principal spillway system is capable of handling less than 20 percent of the PMF. As a low hazard structure, the DNR requires the spillway system to be capable of passing 50 percent. In order to accomplish this capability, the current 30 feet wide spillway need to be increased to 93 feet, or the dam needs to be raised approximately 15.5 feet. There are numerous combinations of these two dimensions that could be considered.

The cost of increasing the spillway to 93 feet is approximately \$650,000. The cost of raising the dam 15.5 feet is approximately \$1,000,000. Raising the dam by 15.5 feet must be carefully evaluated. Checking the relative elevations of home entry points in

comparison to a raised dam height was not part of this study. It is possible that an increased dam height could cause water to enter some homes during large storm events.

Another alternative is to repair the current spillway and armor the embankment to allow overtopping. The cost of armoring the embankment is approximately \$450,000.

Summary of Cost Alternatives and Recommendations

Cost to repair existing spillway - \$150,000
(Will not meet DNR 50% PMF criteria)

Cost to upgrade spillway by widening - \$650,000

Cost to upgrade system by raising the dam - \$1,000,000

Cost to upgrade the system by armoring the dam - \$600,000

All of the alternatives will result in a temporary loss of the lake for up to one year and loss of fishing, if allowed, for up to three years.

The Department of Natural Resources has taken an inconsistent approach to both public and private dam repairs in the past. Currently they are in the process of upgrading their dams, so at some point they most likely will take a more active approach to requiring private dams to be upgraded. However, low hazard dams most likely will remain a low priority as high and significant hazard dams pose a greater threat to the public.

Other factors to consider include the following:

The possibility that downstream development may some day cause a reclassification of your dam to a higher risk rating.

Choosing the do nothing alternative or the repair only alternative could subject you to future action by the DNR.

Electing one of the upgrades could become obsolete if the dam is reclassified in the future, requiring a higher spillway system rating.

The repair only cost estimate is based on what could be seen and hidden costs could increase the cost substantially. The repair only cost should be considered a minimum, not a maximum, cost.

Based on the visual investigation, the dam and spillway system do not appear to be in danger of imminent failure. However, that is no guarantee that failure could not happen immediately. Hidden defects or an intense storm event could result in failure.

We recommend that your organization begin a discussion with the DNR to determine

We recommend that your organization begin a discussion with the DNR to determine the extent of repairs or upgrading that are acceptable to them and a time frame for the work that meets the financial ability of your organization.

BASE RUN
EXISTING CONDITIONS

LINE	ID1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID	HYDROLOGIC MODEL FOR TRADERS POINT LAKE
2	ID	USING SCS METHOD FOR LOSS RATE AND DIMENSIONLESS UNIT HYDROGRAPH
3	ID	
4	ID	*****ESTIMATING % OF PMP RUNOFF DAM CAN CONTROL WITHOUT OVERTOPPING*****
5	ID	CHECKING ONLY 6-HOUR STORM WHICH CONTROLS
6	ID	
7	ID	HUFF 2ND QUARTILE DISTRIBUTION USED FOR 6-HOUR DURATION STORM
8	ID	
*** FREE ***		
9	IT	18 01JAN02 0 250 2000
10	IO	4
11	JR	FLOW .1 .2 .3 .4 .5 .6 .7 .8 1.0
12	KK	STA1
13	KM	TRADERS POINT LAKE 6-HOUR HYDROGRAPH
14	BA	1.63 0
15	PB	27.05
16	PC	0.0 .0280 .0660 .1170 .1813 .2699 .3585 .4440 .5294 .6040
17	PC	.6786 .7219 .7652 .8017 .8381 .8724 .9067 .9328 .9589 .9785
18	PC	1.0
19	LS	0 93
20	UD	2.7
21	KK	STA2
22	KM	ROUTE 6-HR STORM THROUGH LAKE
23	RS	1 ELEV 100 0
24	SA	10 11
25	SE	100 104.5
26	SO	0 32 87 153 227 305 385 465 544 619
27	SE	100 100.5 101 101.5 102 102.5 103 103.5 104 104.5
28	SS	100 0 3.09 1.5
29	ST	104.5 300 3.09 1.5
30	ZZ	

UNIT HYDROGRAPH									
47 END-OF-PERIOD ORDINATES									
9.	30.	58.	95.	144.	197.	238.	264.	275.	275.
264.	245.	223.	195.	162.	132.	110.	92.	77.	67.
56.	48.	40.	34.	29.	24.	20.	17.	14.	12.
10.	9.	7.	6.	5.	4.	4.	3.	3.	2.
2.	2.	1.	1.	1.	0.	0.			

21 KK

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ROUTE 6-HR STORM THROUGH LAKE

HYDROGRAPH ROUTING DATA

23 RS	STORAGE ROUTING									
	NSTPS	1	NUMBER OF SUBREACHES							
	ITYP	ELEV	TYPE OF INITIAL CONDITION							
	RSVRIC	100.00	INITIAL CONDITION							
	X	.00	WORKING R AND D COEFFICIENT							
24 SA	AREA	10.0	11.0							
25 SE	ELEVATION	100.00	104.50							
26 SQ	DISCHARGE	0.	32.	87.	153.	227.	305.	385.	465.	544.
27 SE	ELEVATION	100.00	100.50	101.00	101.50	102.00	102.50	103.00	103.50	104.00
28 SS	SPILLWAY									
	CREL	100.00	SPILLWAY CREST ELEVATION							
	SPWID	.00	SPILLWAY WIDTH							
	COOW	.00	WEIR COEFFICIENT							
	EXPW	1.50	EXPONENT OF HEAD							
29 ST	TOP OF DAM									
	TOPEL	104.50	ELEVATION AT TOP OF DAM							
	DAMWID	300.00	DAM WIDTH							
	COOD	3.09	WEIR COEFFICIENT							
	EXPD	1.50	EXPONENT OF HEAD							

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COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	47.23
ELEVATION	100.00	104.50

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	5.03	10.11	15.25	20.44	25.68	30.99	36.35	41.76	47.23
OUTFLOW	.00	32.00	87.00	153.00	227.00	305.00	385.00	465.00	544.00	619.00
ELEVATION	100.00	100.50	101.00	101.50	102.00	102.50	103.00	103.50	104.00	104.50

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS								
				RATIO 1 .10	RATIO 2 .20	RATIO 3 .30	RATIO 4 .40	RATIO 5 .50	RATIO 6 .60	RATIO 7 .70	RATIO 8 .80	RATIO 9 1.00
HYDROGRAPH AT +	STA1	1.63	1 FLOW TIME	495. 5.10	991. 5.10	1486. 5.10	1981. 5.10	2477. 5.10	2972. 5.10	3467. 5.10	3963. 5.10	4953. 5.10
ROUTED TO +	STA2	1.83	1 FLOW TIME	462. 6.00	988. 5.40	1483. 5.40	1977. 5.40	2471. 5.40	2965. 5.40	3459. 5.40	3954. 5.10	4943. 5.10
** PEAK STAGES IN FEET **												
	1	STAGE		103.48	104.97	105.38	105.68	105.96	106.22	106.46	106.69	107.12
		TIME		6.00	5.40	5.40	5.40	5.40	5.40	5.40	5.10	5.10

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION STA2
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	100.00	100.00	104.50
STORAGE	0.	0.	47.
OUTFLOW	0.	0.	619.

RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.10	103.48	.00	36.	462.	.00	6.00	.00
.20	104.97	.47	52.	988.	3.60	5.40	.00
.30	105.36	.86	57.	1483.	5.10	5.40	.00
.40	105.68	1.18	60.	1977.	6.30	5.40	.00
→ .50	105.96	1.46	64.	2471.	6.90	5.40	.00
.60	106.22	1.72	66.	2965.	7.50	5.40	.00
.70	106.46	1.96	69.	3459.	7.80	5.40	.00
.80	106.69	2.19	72.	3954.	8.10	5.10	.00
1.00	107.12	2.62	77.	4943.	8.70	5.10	.00

*** NORMAL END OF HEC-1 ***

EXPANDED SPILLWAY

LINE	ID1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID	HYDROLOGIC MODEL FOR TRADERS POINT LAKE
2	ID	USING SCS METHOD FOR LOSS RATE AND DIMENSIONLESS UNIT HYDROGRAPH
3	ID	
4	ID	*****ESTIMATING % OF PMP RUNOFF DAM CAN CONTROL WITHOUT OVERTOPPING*****
5	ID	CHECKING ONLY 6-HOUR STORM WHICH CONTROLS
6	ID	
7	ID	HUFF 2ND QUANTILE DISTRIBUTION USED FOR 6-HOUR DURATION STORM
8	ID	
*** FREE ***		
9	IT	18 01JAN02 0 250 2000
10	IO	4
11	JR	FLOW .1 .2 .3 .4 .5 .6 .7 .8 1.0
12	KK	STA1
13	KM	TRADERS POINT LAKE 6-HOUR HYDROGRAPH
14	BA	1.63 0
15	PB	27.05
16	PC	0.0 .0280 .0660 .1170 .1813 .2699 .3585 .4440 .5294 .6040
17	PC	.6786 .7219 .7652 .8017 .8381 .8724 .9067 .9328 .9589 .9795
18	PC	1.0
19	LS	0 93
20	UD	2.7
21	KK	STA2
22	KM	ROUTE 6-HR STORM THROUGH LAKE
23	RS	1 ELEV 100 0
24	SA	10 11
25	SE	100 104.5
26	SO	0 100 281 511 778 1075 1397 1740 2101 2478
27	SE	100 100.5 101 101.5 102 102.5 103 103.5 104 104.5
28	SS	100 0 3.09 1.5
29	ST	104.5 300 3.09 1.5
30	ZZ	

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* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* SEPTEMBER 1990 *
* VERSION 4.0 *
* RUN DATE 01/25/2008 TIME 13:37:10 *
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.....
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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HYDROLOGIC MODEL FOR TRADERS POINT LAKE
USING SCS METHOD FOR LOSS RATE AND DIMENSIONLESS UNIT HYDROGRAPH

*****ESTIMATING % OF PMP RUNOFF DAM CAN CONTROL WITHOUT OVERTOPPING*****
CHECKING ONLY 6-HOUR STORM WHICH CONTROLS

HUFF 2ND QUARTILE DISTRIBUTION USED FOR 6-HOUR DURATION STORM

10 IO OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL
IPLOT 0 PLOT CONTROL
OSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 18 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN 2 STARTING DATE
ITIME 0000 STARTING TIME
NO 250 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 4JAN 2 ENDING DATE
NDTIME 0242 ENDING TIME
ICENT 20 CENTURY MARK

COMPUTATION INTERVAL .30 HOURS
TOTAL TIME BASE 74.70 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF RUNOFF
.10 .20 .30 .40 .50 .60 .70 .80 1.00

12 KK

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* STA1 *
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TRADERS POINT LAKE 6-HOUR HYDROGRAPH

SUBBASIN RUNOFF DATA

14 BA SUBBASIN CHARACTERISTICS
TAREA 1.63 SUBBASIN AREA

PRECIPITATION DATA

15 PB STORM 27.05 BASIN TOTAL PRECIPITATION

16 PI INCREMENTAL PRECIPITATION PATTERN
.03 .04 .05 .06 .09 .09 .09 .09 .07 .07
.04 .04 .04 .04 .03 .03 .03 .03 .02 .02

19 LS SCS LOSS RATE
STRTL .15 INITIAL ABSTRACTION
CRVNBR 93.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

20 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 2.70 LAG

UNIT HYDROGRAPH										
47 END-OF-PERIOD ORDINATES										
9.	30.	58.	95.	144.	197.	238.	264.	275.	275.	
264.	245.	223.	195.	162.	132.	110.	92.	77.	67.	
56.	48.	40.	34.	28.	24.	20.	17.	14.	12.	
10.	9.	7.	6.	5.	4.	4.	3.	3.	2.	
2.	2.	1.	1.	1.	0.	0.				

21 KK

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*****
*           *
*   STA2   *
*           *
*****

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ROUTE 6-HR STORM THROUGH LAKE

HYDROGRAPH ROUTING DATA

23 RS	STORAGE ROUTING										
	NSTPS	1	NUMBER OF SUBREACHES								
	ITYP		ELEV TYPE OF INITIAL CONDITION								
	RSVRIC	100.00	INITIAL CONDITION								
	X	.00	WORKING R AND D COEFFICIENT								
24 SA	AREA	10.0	11.0								
25 SE	ELEVATION	100.00	104.50								
26 SQ	DISCHARGE	0.	100.	281.	511.	778.	1075.	1397.	1740.	2101.	2478.
27 SE	ELEVATION	100.00	100.50	101.00	101.50	102.00	102.50	103.00	103.50	104.00	104.50
28 SS	SPILLWAY										
	CREL	100.00	SPILLWAY CREST ELEVATION								
	SPWID	.00	SPILLWAY WIDTH								
	COOW	.00	WEIR COEFFICIENT								
	EXPW	1.50	EXPONENT OF HEAD								
29 ST	TOP OF DAM										
	TOPEL	104.50	ELEVATION AT TOP OF DAM								
	DAMWID	300.00	DAM WIDTH								
	COOD	3.09	WEIR COEFFICIENT								
	EXPD	1.50	EXPONENT OF HEAD								

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	47.23
ELEVATION	100.00	104.50

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	5.03	10.11	15.25	20.44	25.68	30.99	36.35	41.76	47.23
OUTFLOW	.00	100.00	281.00	511.00	778.00	1075.00	1397.00	1740.00	2101.00	2478.00
ELEVATION	100.00	100.50	101.00	101.50	102.00	102.50	103.00	103.50	104.00	104.50

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION STA2
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	100.00	100.00	104.50
STORAGE	0.	0.	47.
OUTFLOW	0.	0.	2478.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.10	101.46	.00	15.	490.	.00	5.40	.00
.20	102.35	.00	24.	986.	.00	5.40	.00
.30	103.12	.00	32.	1481.	.00	5.40	.00
.40	103.83	.00	40.	1975.	.00	5.40	.00
→.50	104.48	.00	47.	2463.	.00	5.40	.00
.60	104.87	.37	51.	2966.	2.40	5.40	.00
.70	105.15	.65	54.	3460.	3.60	5.40	.00
.80	105.40	.90	57.	3953.	4.50	5.40	.00
1.00	105.85	1.35	62.	4943.	5.40	5.10	.00

*** NORMAL END OF HEC-1 ***

RAISED DAM HEIGHT

```

LINE      ID .....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID  HYDROLOGIC MODEL FOR TRADERS POINT LAKE
2         ID  USING SCS METHOD FOR LOSS RATE AND DIMENSIONLESS UNIT HYDROGRAPH
3         ID
4         ID  *****ESTIMATING % OF PMP RUNOFF DAM CAN CONTROL WITHOUT OVERTOPPING*****
5         ID  CHECKING ONLY 6-HOUR STORM WHICH CONTROLS
6         ID
7         ID  HUFF 2ND QUANTILE DISTRIBUTION USED FOR 6-HOUR DURATION STORM
8         ID
*** FREE ***
9         IT   18 01JAN02      0    250                2000
10        IO    4
11        JR  FLOW    .1    .2    .3    .4    .5    .6    .7    .8    1.0

12        KK   STA1
13        KM  TRADERS POINT LAKE 6-HOUR HYDROGRAPH
14        BA   1.63      0
15        PB  27.05
16        PC   0.0    .0280  .0660  .1170  .1813  .2699  .3585  .4440  .5294  .6040
17        PC  .6786  .7219  .7652  .8017  .8381  .8724  .9067  .9328  .9589  .9795
18        PC   1.0
19        LS    0      93
20        UD   2.7

21        KK   STA2
22        KM  ROUTE 6-HR STORM THROUGH LAKE
23        RS    1    ELEV    100    0
24        SA   10    11    13    14
25        SE   100  104.5  110  115
26        SQ    0    32    87    153    227    305    385    465    544    619
27        SE   100  100.5  101  101.5  102  102.5  103  103.5  104  104.5
28        SS   100    0    3.09  1.5
29        ST  116.5  300  3.09  1.5
30        ZZ
    
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. FLOOD HYDROGRAPH PACKAGE (HEC-1) .
. SEPTEMBER 1990 .
. VERSION 4.0 .
. RUN DATE 01/25/2008 TIME 13:55:18 .
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. U.S. ARMY CORPS OF ENGINEERS .
. HYDROLOGIC ENGINEERING CENTER .
. 609 SECOND STREET .
. DAVIS, CALIFORNIA 95616 .
. (916) 756-1104 .
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HYDROLOGIC MODEL FOR TRADERS POINT LAKE
 USING SCS METHOD FOR LOSS RATE AND DIMENSIONLESS UNIT HYDROGRAPH

*****ESTIMATING % OF PMP RUNOFF DAM CAN CONTROL WITHOUT OVERTOPPING*****
 CHECKING ONLY 6-HOUR STORM WHICH CONTROLS

HUFF 2ND QUANTILE DISTRIBUTION USED FOR 6-HOUR DURATION STORM

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10 IO OUTPUT CONTROL VARIABLES
      IPRNT      4 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      OSCAL      0. HYDROGRAPH PLOT SCALE

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IT HYDROGRAPH TIME DATA
   NMIN      18 MINUTES IN COMPUTATION INTERVAL
   IDATE     1JAN 2 STARTING DATE
   ITIME     0000 STARTING TIME
   ND        250 NUMBER OF HYDROGRAPH ORDINATES
   NDDATE    4JAN 2 ENDING DATE
   NOTIME    0242 ENDING TIME
   ICENT     20 CENTURY MARK

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      COMPUTATION INTERVAL .30 HOURS
      TOTAL TIME BASE     74.70 HOURS

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ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE        DEGREES FAHRENHEIT

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JP MULTI-PLAN OPTION
   NPLAN      1 NUMBER OF PLANS

```

```

JR MULTI-RATIO OPTION
   RATIOS OF RUNOFF
   .10 .20 .30 .40 .50 .60 .70 .80 1.00

```

12 KK

```

.....
. STA1 .
.....

```

TRADERS POINT LAKE 6-HOUR HYDROGRAPH

SUBBASIN RUNOFF DATA

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14 BA SUBBASIN CHARACTERISTICS
      TAREA      1.83 SUBBASIN AREA

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PRECIPITATION DATA

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15 PB STORM      27.05 BASIN TOTAL PRECIPITATION

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16 PI INCREMENTAL PRECIPITATION PATTERN
      .03 .04 .05 .06 .09 .09 .09 .09 .07 .07
      .04 .04 .04 .04 .03 .03 .03 .03 .02 .02

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19 LS SCS LOSS RATE
      STRTL      .15 INITIAL ABSTRACTION
      CRVNBR     93.00 CURVE NUMBER
      RTIMP      .00 PERCENT IMPERVIOUS AREA

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20 UD SCS DIMENSIONLESS UNITGRAPH
      TLAG      2.70 LAG

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PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS									
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	RATIO 7	RATIO 8	RATIO 9	
				.10	.20	.30	.40	.50	.60	.70	.80	1.00	
HYDROGRAPH AT +	STA1	1.63	1	FLOW TIME	495. 5.10	991. 5.10	1486. 5.10	1981. 5.10	2477. 5.10	2972. 5.10	3487. 5.10	3963. 5.10	4953. 5.10
ROUTED TO +	STA2	1.63	1	FLOW TIME	462. 6.00	914. 6.00	1359. 6.30	1800. 6.30	2236. 6.30	2904. 5.70	3492. 5.10	3956. 5.40	4942. 5.40
				** PEAK STAGES IN FEET **									
			1	STAGE TIME	103.48 6.00	106.46 6.00	109.43 6.30	112.37 6.30	115.28 6.30	117.07 5.70	117.50 5.10	117.78 5.40	118.31 5.40

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION STA2
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	100.00	100.00	116.50
STORAGE	0.	0.	202.
OUTFLOW	0.	0.	2419.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.10	103.48	.00	36.	462.	.00	6.00	.00
.20	106.46	.00	70.	914.	.00	6.00	.00
.30	109.43	.00	106.	1359.	.00	6.30	.00
.40	112.37	.00	145.	1800.	.00	6.30	.00
→ .50	115.28	.00	185.	2236.	.00	6.30	.00
.60	117.07	.57	210.	2904.	1.80	5.70	.00
.70	117.50	1.00	216.	3492.	3.00	5.10	.00
.80	117.78	1.28	220.	3956.	3.60	5.40	.00
1.00	118.31	1.81	228.	4942.	4.50	5.40	.00

*** NORMAL END OF HEC-1 ***

