

Formula Sheet for all Wastewater Operator Exams
Revised 3/17

F001

$$\text{Surface area of a pond, acres} = \frac{\text{Length, ft} \times \text{Width, ft}}{43560}$$

F002

$$\text{Volume of a pond, MG} = \left[\frac{(\text{Surface area, sf}) \times (\text{Bottom area, sf})}{2} \right] \times (\text{Depth, ft}) \times \left(\frac{7.48}{1,000,000} \right)$$

F004

$$\text{BOD removal efficiency, \%} = \left(\frac{\text{Influent BOD, mg/L} - \text{Effluent BOD, mg/L}}{\text{Influent BOD, mg/L}} \right) \times 100\%$$

F008

$$\text{Theoretical detention time of a pond, days} = \frac{\text{Volume of the pond, MG}}{\text{Flow rate, MGD}}$$

F011

$$\text{Removal efficiency, \%} = \left(\frac{\text{Influent concentration} - \text{Effluent concentration}}{\text{Influent concentration}} \right) \times 100\%$$

F012

$$\text{Solids, lbs} = (\text{Volume, MG}) \times (\text{MLSS, mg/L}) \times (8.34)$$

F016

$$\text{Average flow rate, MGD} = \frac{(\text{Final flow, MG}) - (\text{Initial flow, MG})}{\text{Time elapsed, days}}$$

F017

$$\text{BOD loading, lbs/day} = (\text{Flow rate, MGD}) \times (\text{BOD, mg/L}) \times 8.34$$

F018

$$\text{TSS removal efficiency, \%} = \left(\frac{\text{Influent TSS} - \text{Effluent TSS}}{\text{Influent TSS}} \right) \times 100\%$$

F020

$$\text{Volume of sample needed for a BOD test bottle, mL} = \frac{1200}{\text{Estimated BOD of the sample, mg/L}}$$

F021

$$\text{BOD, mg/L} = \frac{(\text{Initial D.O., mg/L} - \text{Final D.O., mg/L}) \times 300 \text{ mL}}{\text{Sample volume, mL}}$$

F022

Chlorine feed rate, lbs/day = (Flow, MGD) x (Dosage, mg/L) x (8.34)

F023

TSS test results, mg/L = $\left(\frac{\text{Net dry weight, mg}}{\text{Sample volume, mL}} \right) \times 1000 \text{ mL/L}$

Or

TSS test results, mg/L = $\left(\frac{\text{Net dry weight, g}}{\text{Sample volume, mL}} \right) \times 1,000,000 \text{ mL/L}$

F030

Pump capacity, gpm = $\frac{(\text{Width, ft}) \times (\text{Length, ft}) \times (\text{Draw-down, ft}) \times 7.48}{\text{Time of draw-down in minutes}}$

F030B

Increased flow = $\frac{(\text{New pipe diameter, inch})^2}{(\text{Old pipe diameter, inch})^2}$

F030C

Flow rate in a pipe, gpd =

$$\left[\frac{(\text{Pipe diameter, inches})^2}{(12 \text{ in/ft})^2} \right] \times 0.785 \times (\text{Velocity, ft/sec}) \times 60 \text{ sec/min} \times 1440 \text{ min/day} \times 7.48 \text{ gal/cf}$$

F032

Desired suspended solids, lbs = (Sludge age, days) x (Primary effluent solids, lb/day)

F033

Volume per stroke, gal/stroke = $\left[\frac{(0.785) \times (\text{Diameter, inches})^2}{12^2} \right] \times \left[\frac{(\text{Stroke, inches}) \times (7.48)}{12} \right]$

F034

Total dry solids, lbs = $\frac{(\text{Raw sludge, gal}) \times (\text{Total solids, \%}) \times (8.34)}{100\%}$

F035

MLSS, lbs = (Aeration volume, MG) x (MLSS conc, mg/L) x (8.34)

F037

Digestion time, days = $\frac{\text{Digester volume, gal}}{\text{Flow, gpd}}$

F038

$$\text{Phosphorus (P) removal, \%} = \left(\frac{\text{Influent P, mg/L} - \text{Effluent P, mg/L}}{\text{Influent P, mg/L}} \right) \times 100\%$$

F039

$$\text{Sludge applied, gal} = \frac{(\text{Area, sf}) \times (\text{Depth of application, in}) \times (7.48)}{12 \text{ in/ft}}$$

F040

$$\text{Pollutant emission rate, lbs/day} = \frac{(\text{Flow, gpd}) \times (\text{Pollutant conc., mg/L}) \times (3.785 \text{ L/gal})}{453,600 \text{ mg/lb}}$$

F043

$$\text{Chemical application rate, lbs/day} = (\text{Flow, MGD}) \times (\text{Chemical dosage, mg/L}) \times 8.34$$

F045

$$\text{Flux, gpd/sf} = \frac{(\text{Flow rate, gpm}) \times (60 \text{ min/hr}) \times (24 \text{ hr/day})}{\text{Surface area of membrane, sf}}$$

F047

$$\text{New, or actual, WAS flow rate, MGD} = \frac{(\text{Calculated WAS flow, MGD}) \times (24 \text{ hr/day})}{\text{Actual hours of sludge wasting, hr/day}}$$

F048

$$\text{Solids produced, lbs/day} = (\text{BOD removed, lbs/day}) \times (\text{Yield factor})$$

F050

$$\text{Primary sludge, lbs/day} = (\text{Flow rate, MGD}) \times (\text{Inflow SS, mg/L} - \text{Effluent SS, mg/L}) \times 8.34$$

F052

$$\text{Hydraulic loading of a DAF unit, gpd/sf} = \frac{(\text{Inflow rate, gpm}) \times (1440)}{\text{Liquid surface area, sf}}$$

F053

$$\text{Solids loading to a centrifuge, lbs/hr} = \frac{(\text{Sludge flow rate, gal/hr}) \times (\text{Sludge conc \%}) \times 8.34 \text{ lbs/gal}}{100\%}$$

F054

$$\text{Efficiency of solids removal, \%} = \left(\frac{\text{Influent SS, \%} - \text{Effluent SS, \%}}{\text{Influent SS, \%}} \right) \times 100\%$$

F055

$$\text{Dry polymer, lbs} = (\text{Volume of solution, gal}) \times \left(\frac{\text{Polymer concentration, \%}}{100\%} \right) \times (8.34 \text{ lb/gal})$$

F058

$$\text{Pumping rate, gpm} = \frac{(\text{Volume, cf}) \times (7.48 \text{ gal/cf})}{\text{Time, min}}$$

F061

$$\text{Surface loading, gpd/sf} = \frac{\text{Flow, gpd}}{\text{Surface area, sf}}$$

F062

$$\text{Solids loading, lbs/day/sf} = \frac{(\text{Flow, MGD}) \times (\text{TSS, mg/L}) \times (8.34)}{\text{Surface area, sf}}$$

F063

$$\text{Sludge age} = \frac{\text{TSS in aerator, lbs}}{\text{TSS in primary effluent, lbs/day}}$$

F064

$$\text{F/M} = \frac{\text{lbs BOD/day to aeration tank}}{\text{lbs of MLVSS under aeration}}$$

F065

Waste sludge pumping rate, MGD =

$$\text{Current pump rate, MGD} + \left[\frac{(\text{Difference in aerator sludge inventory, lbs})}{(\text{RAS concentration, mg/L}) \times 8.34} \right]$$

F066

$$\text{MCRT, days} = \frac{\text{MLSS in aeration tank, lbs}}{(\text{TSS wasted, lbs/day}) + (\text{TSS in effluent, lbs/day})}$$

F068

$$\text{MLVSS, mg/L} = \frac{\text{BOD Loading from primary, lbs/day}}{(\text{F/M Ratio}) \times (\text{Aerator volume, MG}) \times (8.34)}$$

F069

$$\text{Return sludge rate, MGD} = \frac{\text{Settled solids, mL} \times (\text{Flow, MGD})}{(1000 \text{ mL} - \text{Settled solids, mL})}$$

F073

$$\text{SO}_2 \text{ feed, lbs/day} = (\text{Flow, MGD}) \times (\text{Residual chlorine, mg/L} + \text{SO}_2 \text{ overdose, mg/L}) \times (8.34)$$

F074

Chlorine demand, mg/L = (Chlorine dose, mg/L) - (Chlorine residual, mg/L)

F076

Polymer dose, mg/L =
$$\frac{(\text{Polymer delivery rate, gpm}) \times (\text{Polymer, lbs/gal}) \times (1,000,000)}{(\text{Flow, gpm}) \times (8.34)}$$

F077

Polymer dose, mg/L =
$$\frac{(\text{Polymer feed rate, lbs/day}) \times (1,000,000)}{(\text{Flow, gpm}) \times (1440) \times (8.34)}$$

F078

Volume of seed sludge, gal = (Volume of digester, gal) x (% seed)

F081

Total settleable solids to pump to digester, gpd = (Sludge removed, mL) x (Flow, MGD) x (1000)

F082

% reduction of volatile matter, % =
$$\frac{(\text{In} - \text{Out}) \times (100)}{\text{In} - [(\text{In}) \times (\text{Out})]}$$
 ("in" and "out" in fraction, not in %)

F083

% reduction of volatile matter, % =
$$\left[\frac{(\text{Initial volatile matter, lbs}) - (\text{Final volatile matter, lbs})}{\text{Initial volatile matter, lbs}} \right] \times 100 \%$$

F087

Seed correction per 1.0 mL of seed =
$$\frac{\text{Initial D.O.} - \text{Final D.O.}}{\text{mL of seed in bottle}}$$

and

BOD₅, mg/L =
$$\left\{ \frac{[(\text{Initial DO, mg/L}) - (\text{Final DO, mg/L})] - (\text{Seed correction, mg/L})}{\text{Sample volume, mL}} \right\} \times 300 \text{ mL}$$

F088

Volume diluted, mL =
$$\frac{(\text{Target normality}) \times (\text{Target volume, mL})}{\text{Stock acid normality}}$$

F091

Sludge flow, MGD =
$$\frac{(\text{Thickener loading, lbs/day/sf}) \times (\text{Surface area, sf})}{(8.34) \times (10,000) \times (\% \text{ solids})}$$

F092

Desired lbs of solids in aeration tank = (Daily solids addition, lbs/day) x (Sludge age, days)

F094

$$\text{New digestion time, days} = \frac{(\text{Digester volume, gal}) \times (\text{Increase in sludge conc. \%} - \text{Initial sludge conc. \%})}{(\text{Initial sludge flow, gpd}) \times (\text{Initial sludge conc. \%})}$$

F096

$$\text{Volume of working solution, mL} = \frac{(\text{Beaker volume, mL}) \times (\text{Dosage, mg/L})}{(\text{Stock solution conc, \%}) \times (10,000)}$$

F097

$$\text{Chemical feed rate, gph} = \frac{(\text{Flow, MGD}) \times (\text{Dosage, mg/L}) \times 100\%}{(\text{Solution strength, \%}) \times (24 \text{ hr/day})}$$

F098

$$\text{Surface loading rate, gpd/sf} = \frac{(\text{Flow rate, MGD}) \times (1,000,000 \text{ gal/MG})}{(\text{Diameter, ft})^2 \times (0.785)}$$

F099

$$\text{Polymer dosage, mg/L} = \frac{(\text{Polymer pumping rate, gpm}) \times (\text{Polymer conc. lbs/gal}) \times (1,000,000)}{(\text{Sludge flow rate, gpm}) \times (8.34 \text{ lbs/gal})}$$

F100

$$\text{Retention \%} = \frac{(\text{Retentate conc., mg/L}) - (\text{Permeate conc., mg/L})}{\text{Retentate conc., mg/L}} \times 100\%$$

F101

$$\text{Average transmembrane pressure, psi} = \frac{(\text{Inlet pressure, psi} + \text{Outlet pressure, psi}) - \text{Permeate pressure, psi}}{2}$$

F103

$$\text{RAS, MGD} = \frac{(\text{Settled volume, mL/L}) \times (\text{Influent flow rate, MGD})}{(1000 \text{ mL/L}) - (\text{Settled volume, mL/L})}$$

F105

$$\text{Sludge age, days} = \frac{(\text{Tank volume, MG}) \times (\text{MLSS, mg/L})}{(\text{Inflowrate, MGD}) \times (\text{Primary effluent SS, mg/L})}$$

F106

$$\text{F/M, lb COD/day per lb MLVSS} = \frac{(\text{Flow, MGD}) \times (\text{COD, mg/L}) \times (8.34 \text{ lbs/gal})}{(\text{Solids under aeration, lbs}) \times (\text{Volatile fraction})}$$

F108

$$\text{Phosphorus to be added, lbs/day} = [\text{BOD lbs/day} \times \text{P/BOD (desired ratio)}] - (\text{P in wastewater, lbs})$$

F110

Desired COD loading, lbs/day = (COD loading rate, lbs COD/lbs VS) x (VS, lbs)

F111

Sludge produced, lbs/day =
(Flow, MGD) x (Influent BOD, mg/L - Effluent BOD, mg/L) x (8.34 x yield factor)

F112

Thickened sludge volume, gal/day = $\left(\frac{\text{Sludge, lbs/day}}{8.34 \text{ lbs/gal}} \right) \times \left(\frac{100\%}{\text{Sludge solids concentration, \%}} \right)$

F114

Solids loading, lbs/hr/sf = $\frac{(\text{Flow, gpm}) \times (60) \times (8.34 \text{ lbs/gal}) \times (\text{SS}\%)}{(\text{Liquid surface area, sf}) \times (100\%)}$

F115

Air to solids ratio = $\frac{(\text{Air supply rate, cfm}) \times (0.075 \text{ lb/cf}) \times (100\%)}{(\text{Solids feed rate, gpm}) \times (\text{Sludge conc, \%}) \times (8.34 \text{ lbs/gal})}$

F116

Feed time to a centrifuge, min = $\frac{(\text{Storage volume, cf}) \times (\text{Basket sludge conc, \%}) \times (62.4 \text{ lbs/cu ft})}{(\text{Flow, gpm}) \times (\text{Influent solids, \%}) \times (8.34 \text{ lbs/gal})}$

F117

Increase of detention time, days = $\frac{(\text{Aerobic digester volume, gal}) \times (\text{Increase in sludge conc., \%})}{(\text{Initial sludge flow, gpd}) \times (\text{Initial sludge conc., \%})}$

F122

Polymer dosage, lbs/ton = $\frac{(\text{Polymer solution conc, \%}) \times (\text{Polymer added, gpm}) \times (2,000 \text{ lbs/ton})}{(\text{Sludge conc, \%}) \times (\text{Sludge flow rate, gpm})}$

F123

Vacuum filter yield, lbs/hr/sq ft = $\frac{\text{Sludge loading, lbs/day} \times \left(\frac{\text{Recovery, \%}}{100\%} \right)}{(\text{Duration of filter operation, hr/day}) \times (\text{Filter area, sf})}$

F124

Required filter run time, hr/day = $\frac{\text{Sludge solids loading, lbs/day} \times \text{Solids recovery, \%}}{(\text{Filter yield, lbs/hr/sf}) \times (\text{Filter area, sf}) \times (100\%)}$